## Towards Improved Thickness Design Procedures for Foamed Bitumen Stabilised Layers: New Experimental Findings Towards Improved Thickness Design Procedures<br>for Foamed Bitumen Stabilised Layers:<br>New Experimental Findings<br><sub>Didier Bodin, Principal Technology Leader – NTRO</sub><br>Damian Volker, A/Director (Pavement Rehabilitation), Pavements Towards Improved Thickness Design Procedures<br>For Foamed Bitumen Stabilised Layers:<br>New Experimental Findings<br>Didier Bodin, Principal Technology Leader – NTRO<br>Damian Volker, A/Director (Pavement Rehabilitation), Pavements,



**Australian Pavement Recycling** and Stabilisation Conference Designing for Reuse and Resilience

Pullman King George Square, Brisbane . 7th August 2024

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Monash University: Fibre optic sensors support & SPARC Hub collaboration





### **Outline**

- **Background**
- **Scope of the initiative**
- **Effect of temperature and loading speed on FBS modulus**
- **Fatigue characterisation and temperature susceptibility**
- **Innovative laboratory XL-WT testing under field-simulated** conditions
- Conclusions





## Background

- TMR structural design procedure was developed and used at large scale
- Current mix design practice 3. to 3.5 % bitumen & 1.5 to 2% hydrated lime/ fly ash
- **Typical mixtures are rut resistant in early life and beyond (research showed validity up to** 50% RAP )
- Thickness design based on an empirical performance relationship:
	- **Design modulus (derived from mix design) 3-day cured soaked IT modulus of laboratory prepared** specimens adjusted for temperature/loading speed and capped to 2,500 MPa
	- Strains determined from design response to load model (i.e. Circly/AustPads)
	- **Empirical performance relationship**  $\Rightarrow$  **allowable loading**
	- Allowable loading **S** design traffic?
- Method translated to AGPT05:2019 for pavement rehabilitation treatment design
- Reliability factors are not available for FBS pavements





### Towards a performance-based characterisation and design procedure

- Aim at a probabilistic approach consistent with<br>the Austroads Mechanistic-Empirical design<br>procedure for bound materials (AGPT02)<br>• Laboratory-derived performance relationship<br>• Shift factor (calibrate mean lab performan the Austroads Mechanistic-Empirical design procedure for bound materials (AGPT02)
- Laboratory-derived performance relationship
- Shift factor (calibrate mean lab performance on mean field performance)
- **Reliability factors for given design reliability**







### Flexural modulus and fatigue performance

New laboratory characterisation procedures

- **90-days cured laboratory-prepared beams** (100 x 100 x 400 mm) Flexural modulus and fatigue performance of the Margaret Seams<br>
Flexural modulus (T, f,  $\varepsilon \le 50 \mu\text{E}$ )<br>
Flexural fatigue (T°C, f = 10Hz, varying stress)
- **4pt bending testing conditions**
- 
- 



Sydney, NSW.





### Laboratory flexural fatigue relationships

- Austroads report (AP-R666-22)
- B different mixes tested to investigate fundamental parameters affecting fatigue performance
	- Effect of modulus
	- Effect of the bitumen content
	- Effect of strength
- **Testing at 20°C**
- On going NACOE/Austroads research 1.0E+03 to consolidate the findings<br>
Source: Zhalehioo (2022)







### Scope of the research

- Undertake fatigue testing on two typical FBS mixes representative of TMR practice
- Assess effect of temperature and loading speed on flexural modulus
- **Perform fatigue testing and assess sensitivity to temperature**
- Better understanding lab to field shift factor based on XL-WT test





### Effect of loading speed/temperature on FBS materials modulus

- Similarly to asphalt and all bituminous materials, FBS mixes are sensitive to temperature and loading speed (viscoelastic material)  $\Rightarrow$  New lab study
- FBS mixtures
	- Type 2.1 crushed rock  $(x2)$
	- Bitumen content 3.5%
	- BItumen content 3.5%<br>
	Secondary binder 1.5% (50/50 Hydrated lime/Fly ash)<br>
	BO-day cured lab-manufactured beams<br>
	BO-day cured lab-manufactured beams
- 90-day cured lab-manufactured beams
- 'Master curve' testing:
	- Temperatures = 20, 25 and 35ºC
	- Frequency sweep  $f = 1, 3, 5, 10, 15, 20$  Hz







### Effect of temperature on the flexural modulus









### Effect of loading frequency of modulus

#### **Experiment 2 Mixtures + Austroads (2022) data**







### Fatigue Testing at 25°C







### Fatigue relationship SDE / Model

#### **Strain damage exponent (SDE)**



#### Laboratory model predicts higher lives than measured





### Effect of temperature on fatigue

Use similar testing protocol at varying temperature (20, 25 and 35ºC)



Drop in fatigue about 4 to 5 times between 20 to 35 °C lower than previous findings showed lives more than 10 times greater for a 10ºC increase





### WT testing to better simulate field conditions

- **Flexural fatigue** 
	- Uniaxial loading (i.e. bending)
	- Unconfined specimen
- **Field** 
	- Rolling wheel load & 3D stress/strain state
	- Material confined in the layer by surrounding material
- Extra-large wheel tracker selected tobetter simulate field conditions
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	- 20kN rolling wheel load<br>Confinement (i.e slab specimen confined in a<br>steel mould)



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Source: NTRO (2023)



# Extra-Large Wheel-tracker<br>pavement material fatigue<br>• XL-WT - originally developed for<br>• Used to characterise cracking types of Extra-Large Wheel-tracker for simulating pavement material fatigue Mould frame 700 mm

- unbound granular materials
- **Used to characterise cracking types of** lightly bound stabilised materials (AP-R640-20) XL-WT - originally developed for<br>
unbound granular materials<br>
Used to characterise cracking types of<br>
lightly bound stabilised materials (AP-<br>
R640-20)<br>
Allows in-flight response to load<br>
monitoring<br>
High load capacity wit
- **Allows in-flight response to load** monitoring
- High load capacity with slab testing





### Optic fiber sensors implementation

- **Understanding tensile strain** at the bottom of the slab
	- **Longitudinal**
	- **Transverse**
- **Installation at the bottom &** top of the slab
- **Evaluate the technology** robustness







### Small strain response to load testing

**Determine load vs strain relationship (testing for 100 cycles)** 



- **Linear strain / displacement response with load**
- Tensile strain  $\varepsilon_{xx} \varepsilon_{yy}$  consistent  $\Rightarrow$  bi-directional tensile strain





### Life expectancy from flexural fatigue

- Load magnitude 4.5 kN
- **Life predicted based on flexural fatigue results**







### Multi-stage testing





- $\rightarrow$  Mix 2 (x=0,y=0) during fatigue test
- Mix  $2(x=0,y=0)$  during 100 cycles with 4.5 kN
- $\rightarrow$  Mix 1 (x=0,y=0) during fatigue test
- Mix 1  $(x=0,y=0)$  during 100 cycles with 4.5 kN
- **Number of load repetition far exceeded prediction from flexural testing**





### Conclusion

- Effect of temperature on modulus and loading speed found lower than currently assumed
- Improved assessment of fatigue performance temperature susceptibility
- Use of fibre optic cables gives an interesting insight into the flexural response under rolling wheel-load
- XL-WT testing provided a confined and 3D stress representing the field
- Shift factor between flexural testing and WT is far greater than 7

#### Continuing research

- Assessment of field performance to evaluate the lab-to-field shift factor
- Further ongoing validation of the effect of temperature/loading speed sensitivity and model<br>refinements
- Reliability (i.e. surviving rate) of the fibre optic sensors should be improved





### Thank you

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