Enhancing Long-Term Performance of Unsealed Roads in Australia: The Use of Crushed Rock Treated with Anionic Bituminous Emulsion Enhancing Long-Term Performance of
Unsealed Roads in Australia:
The Use of Crushed Rock Treated with Anionic
Bituminous Emulsion
Asanka de Silva, Arooran Sounthararajah, Hamed Haghighi,
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Australian Pavement Recycling and Stabilisation Conference

Designing for Reuse and Resilience Pullman King George Square, Brisbane . 7th August 2024

Research Objectives

To develop a novel and economical solution for dust level monitoring on unsealed roads

Existing dust monitoring methods **Solution**
 Solution for dust
 Solution for dust

level monitoring on

unsealed roads

Existing dust monitoring methods

Machine learning - semantic segmentation

Machine learning - semantic segmentation

Benchmark dat Benchmark dataset Field experiments

Different machine learning models

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To investigate the effectiveness of bituminous emulsion treatment on crushed rock for enhanced performance

Particle size distribution Atterberg limits To investigate the
effectiveness of
bituminous emulsion
treatment on crushed rock
for enhanced performance
Particle size distribution
Atterberg limits
Soil particle density
Dry density – moisture content relationship
Modif Modified Proctor Gyratory compactor Tensile strength Resilient modulus Soil particle density Ignition oven test Performance against rutting

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Material Characterisation

Particle size Particle size

distribution of

crushed

rock

rock

and
 $\sum_{\substack{g \to 2,25 \\ g \to 2,25}}$ crushed rock

Indirect tensile

resilient modulus:

crushed rock and

bitumen-emulsion

treated crushed tock resilient modulus: \sum_{\pm}^{∞} crushed rock and $\sum_{\underline{5} \atop \underline{3} \atop \underline{3} \bmod 6}$ **bitumen-emulsion** $\frac{5}{9}$ $\frac{300}{250}$ treated crushed tock $\frac{a}{2}$

 240

Compaction curves (modified Proctor and Gyratory compactor)

Indirect tensile strength: crushed rock and bitumenemulsion treated crushed tock

Materials – Crushed Rock Treated With Emulsion^{5/19}
CT Scans 5/19

CT Scans

Microstructure of crushed rock treated with anionic slow set bituminous emulsion.

(a)3D view of 100 mm diameter quarter cut cylindrical sample,

(b) Cross-sectional view of untreated crushed rock,

(c) Cross-sectional view of crushed rock treated with 1% bituminous emulsion,

(d) Cross-sectional view of crushed rock treated with 2% bituminous emulsion,

(e) Cross-sectional view of crushed rock treated with 3% bituminous emulsion.

Wheel tracker testing 6/19

Australian Pavement Recycling and Stabilisation Conference Designing for Reuse and Resilience Pullman King George Square, Brisbane . 7th August 2024 Table 1: OMC and MDD of different mixtures.

	Mixture Binder content $(\%)$		OMC MDD (t/m^3)
		67	2.23
		6.7	2.23
3		6.3	2.26
		6.0	2.24
		6.5	

Table 2: Test conditions.

Wheel tracker testing ctd…

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Wheel tracker 8/19

Mean Profile Deformation

$$
PD_{mean}^{i}(N) = \sum_{j=1}^{n_i} \frac{(m_{ij}(N) - m_{ij}(0))}{n_i} \qquad PD_{max}^{i}(N) = max_{j=1}
$$

Maximum Profile Deformation

$$
E_{mean}(N) = \sum_{i} \frac{(m_{ij}(N) - m_{ij}(0))}{n} \qquad \qquad PD_{max}^i(N) = max_{j=1 \text{ to } n_i} \left(m_{ij}(N) - m_{ij}(0) \right)
$$

 $PD_{mean}^i(N) = i^{th}$ profile mean deformation at cycle N (mm)

 $PD_{max}^i(N) = i^{th}$ profile maximum deformation at cycle N (mm)

Overall Mean Deformation

$$
D_{mean}(N) = \sum_{i=1}^{n_p} \frac{PD_{mean}^i(N)}{n_p}
$$
\n
$$
PRD_{max}^i(N) = max_{j=1 \text{ to } n_i} \left(r_{ij}(N) \right)
$$
\n
$$
PRD_{max}^i(N) = i^{th} \text{ profile maximum rut depth at cycle } N \text{ (m)}
$$
\n
$$
PRD_{max}^i(N) = i^{th} \text{ profile maximum rut depth at cycle } N \text{ (m)}
$$

Overall Maximum Deformation

$$
D_{max}(N) = \sum_{i=1}^{n_p} \frac{PD_{max}^i(N)}{n_p}
$$
 RD_{ma}

 $D_{mean}(N) = overall$ mean deformation at cycle N (mm) n_p = number of profiles $D_{max}(N) =$ overall maximum deformation at cycle N (mm) Dverall Maximum Deformation
 $D_{max}(N) = \sum_{i=1}^{n_p} \frac{PD_{max}^i(N)}{n_p}$ $RD_{max}(N)$
 $RD_{max}(N) = overall \ mean \ deformation \ at \ cycle \ N \ (mm)$
 $_{n_p = number \ of \ pro}^i$
 $_{n_p = number \$

 $PD_{max}^i(N) = i^{th}$ profile maximum deformation at cycle N (mm) $PD_{mean}^i(N) = i^{th}$ profile mean deformation at cycle N (mm)

Maximum Profile Rut Depth

$$
PRD_{max}^i(N) = max_{j=1 \text{ to } n_i} (r_{ij}(N))
$$

 n_p and the proof $PED_{max}^i(N) = i^{th}$ profile maximum rut depth at cycle N (mm) $PSD_{max}^i(N) = i^{th}$ profile maximum rut depth at cycle N (mm)

Maximum Profile Rut Depth
 $PRD_{max}^i(N) = max_{j=1 \text{ to } n_i} (r_{ij}(N))$
 $PRD_{max}^i(N) = i^{th} profile maximum run depth at cycle N (mm)$
 $n_i = number of transverse locations defined for the i^{th} profile measurements$
 $n_i(N) = the distance calculated at the location j and the cycle N between the straight edge and the specimen surface (mm)$
 Overall Maximum Rut Depth
 n_p ppp₁ (1)

Overall Maximum Rut Depth

$$
D_{max}(N) = \sum_{i=1}^{n_p} \frac{PD_{max}^i(N)}{n_p}
$$

$$
RD_{max}(N) = \sum_{i=1}^{n_p} \frac{PRD_{max}^i(N)}{n_p}
$$

 $RD_{max}(N) = overall$ maximum rut depth at cycle N (mm)

 n_p = number of profiles

 $PRD_{ma}^{i} \, \left(N\right)=i^{th}$ profile maximum rut depth at cycle N (mm)

Tyres 11/19

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Surface Deformation by Laser Profilometry

12/19

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Surface Deformation by Laser Profilometry ctd… 13/19

Permanent Deformation by Deflection Sensors 15/19

Permanent Deformation ctd...

Conclusions

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The use of a treaded tyre in contrast to a smooth tyre is highlighted by
observing how the rutting is considerably higher when a treaded tyre was
The results from MT test suggest that bituminous emulsion treatm Conclusions

Conclusions

The use of a treaded tyre in contrast to a smooth tyre is highlighted by

observing how the rutting is considerably higher when a treaded tyre was

used.

The results from WT test suggest that bit used.

The results from WT test suggest that bituminous emulsion treatment considerably improves the rutting performance of the pavement.

Crushed rock treated with the 3% bituminous emulsion showed the lowest overall maximum rut depth and overall mean deformation whereas untreated crushed rock showed the highest overall maximum rut depth and overall mean deformation.

The results of this study show that the bituminous emulsion treatment is effective in terms of the long-term performance of unsealed road pavements.

Publications

- er and De Silva, Arooran Sounthararajah, Troyee Tanu Dutta, David Firth, Jaimi Harrison, Hamed Haghighi,

Jayantha Kodikara, Crushed rock treated with anionic bituminous emulsion for construction of unsealed

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Acknowledgements

Thank you!

